$$
\begin{aligned}
& \text { STRARS } \\
& \text { STREET } \\
& R A \mathbb{R} \mathbb{R} W A Y \\
& \mathbb{C U R V E S}
\end{aligned}
$$



Frog and Switch Dept.


$$
\text { JAN } 81008
$$

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## SPIRALS

for
Street Railway Curves and Easement Curves for

Street Railway Branch-Offs


Complete Formulas and Tables 0

The Pennsylvania Steel Company Steelton, Pa .

FROG AND SWITCH DEPARTMENT

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4 THE PENNSYLVANLA STEEL COMPANY

## LIST OF OFFICES

## of

## The Pennsylvania Steel Company

## GENERAL SALES OFFICE

## Philadelphia, Pa., Girard Trust Building

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HE Spiral System presented in the following pages has been in use by The Pennsylvania Steel Company for the last decade, and has given general satisfaction. It consists of a transition formed of arcs of diminishing radii, and is calculated upon the center line of track, since that is substantially the path followed by the center of gravity of the cars. The purpose of a spiral ending on a short radius street railway curve is not as in steam railroad practice, to enable the super-elevation of the outer rail of curve to be gradually attained, but to reduce the shock due to the change in direction of the car. The switch easements are so designed that a plain curve can be converted
into a branch-off with the minimum disturbance of existing work while retaining standard switches and mates, and some simplification of computation is also obtained. The solutions of the various problems given present sufficient information to enable any data required for the laying out or construction of track to be readily secured.

Problem 1. To select a spiral.
(a) The radius of the main curve must be less than the preceding branch of the spiral, must be more than the next branch would be were it produced, and should nearly equal the latter.
(b) The longer the spiral, the easier the entrance will be. But bear in mind that the main body of the curve should be circular, the spiral simply acting as an entrance to it.
(c) A spiral of less than three branches should not be used.


Problem 2. Given: A circular curve with symmetrical spirals, to find the tangent and external distances.

$$
\begin{aligned}
& \mathrm{O} G=\mathrm{R}+\mathrm{X} \text {-versine } \mathrm{S}^{\circ} \mathrm{R} \text {; } \\
& \mathrm{GS}=\mathrm{Y}-\operatorname{sine} \mathrm{S}^{\circ} \mathrm{R} ;
\end{aligned}
$$

Tangent distance $=0 \mathrm{G} \tan 1 / 2 \Delta+G \mathrm{~S}$;
External distance $=O \mathrm{G}$ ex $\sec 1 / 2 \Delta+X-$ versine $S^{\circ}$ R.


Problem 3
Problem 3. Given: The tangent distance V S, the intersection angle $\Delta$, and the desired length of spiral, to find the radius of the curve. Approximate $\mathrm{R}=$ cotangent $1 / 2 \Delta$ (V S $-1 / 2$ length of spiral). Having selected a spiral by this radius, the exact radius may be found, if required, by the following formula:

$$
\mathrm{R}=\frac{\cos 1 / 2 \Delta(\mathrm{~V} \mathrm{~S}-\mathrm{Y}-\mathrm{X} \tan 1 / 2 \Delta)}{\operatorname{sine}(1 / 2 \Delta-\mathrm{S})} .
$$

Caution-If the result is enough different from the original radius to require a change in the spiral by Problem 1, a second trial must be made.

Problem 4. Given: The intersection angle $\triangle$
and the external distance V H , to find the radius. Approximate to the radius by finding that for a simple curve passing through the point H , and select a spiral for a radius somewhat smaller.

$$
\text { Then } \mathrm{R}=\frac{\mathrm{VH} \cos 1 / 2 \Delta-X}{\cos \mathrm{~S}^{\circ}-\cos 1 / 2 \Delta} \text { (Searle). }
$$

Caution-If the result is enough different from the original radius to require a change in the spiral by Problem 1, a second trial must be made.


Problems 5 and 6
Problem 5. Given: The X and Y for any point on the spiral; to find the deflection from the tangent at the point of spiral.

Tangent deflection angle $=\frac{X}{\bar{Y}}$.
Problem 6. Given: The X and Y for any point on the spiral, to find the long chord.

$$
\text { (a) Long chord }=\frac{Y}{\text { cosine def angle }}
$$

or (b) Long chord $=\sqrt{\mathrm{X}^{2}+\mathrm{Y}^{2}}$.
Problem 7. Given: $X$ and $Y$ for a point on the spiral,- to find $\mathrm{X}^{\prime}$ and $\mathrm{Y}^{\prime}$ on a line parallel to the spiral, and offset the distance $\mathrm{S} \mathrm{S}^{\prime}$ inside the spiral.

$$
\begin{aligned}
& \mathrm{X}^{\prime}=\mathrm{X}-\mathrm{S} \text { S } \mathrm{S}^{\prime} \text { versine } \mathrm{S}^{\circ} ; \\
& \mathrm{Y}^{\prime}=\mathrm{Y}-\mathrm{S} \mathrm{~S}^{\prime} \text { sine } \mathrm{S}^{\circ} .
\end{aligned}
$$

Note-Problems 5 and 6 can then be applied to $\mathrm{X}^{\prime}$ and $\mathrm{Y}^{\prime}$ if it is desired to use deflection angles to lay out the curve.


Problem 7
As these curves will almost invariably be laid out on an offset varying with the gage of the road, the deflections are not figured in the table.

tangent to the circular curve, from which the latter may be laid out in the usual manner.
$\mathrm{V} H=$ see Problem $2 ;$
$\mathrm{V}^{\prime} \mathrm{H}=\mathrm{R}$ ex secant $(1 / 2 \Delta-\mathrm{S}) ;$
$\mathrm{V}^{\prime}=\mathrm{V} H-\mathrm{V}^{\prime} \mathrm{H}$.


Problem 9
Problem 9. General solution for unsymmetrical curves.
$O G=R+X-R$ versine $S^{\circ}$;
-G $\mathrm{S}=\mathrm{Y}-\mathrm{R}$ sine $\mathrm{S}^{\circ}$;
$O G^{\prime}=R+X^{\prime}-R$ versine $S^{\circ}$;
G $\mathrm{S}^{\prime}=\mathrm{Y}-\mathrm{R}$ sine $\mathrm{S}^{\circ \prime}$;
$\mathrm{V} \mathrm{S}=\tan 1 / 2 \Delta \mathrm{OG}+\mathrm{GS}+\frac{\mathrm{OG}^{\prime}-\mathrm{OG}_{\mathrm{G}}}{\operatorname{sine} \Delta} ;$
$V S^{\prime}=\tan 1 / 2 \Delta O G+G^{\prime} S^{\prime} \pm \frac{O G^{\prime}-O G}{\tan \Delta}$.

Note - $\pm$ in above; + if $\Delta$ is more than $90^{\circ}$, and - if $\Delta$ is less than $90^{\circ}$.

$$
\begin{aligned}
\Delta^{\prime} & =\Delta-\left(\mathrm{S}^{\circ}+\mathrm{S}^{\circ \prime}\right) ; \\
\mathrm{V}^{\prime} \mathrm{L} \text { or } \mathrm{V}^{\prime} \mathrm{L}^{\prime} & =\tan \mathrm{V}^{\prime / 2} \Delta^{\prime} \mathrm{R} ; \\
\mathrm{V}^{\prime} \mathrm{B} & =\mathrm{X}+\mathrm{V}^{\prime} \mathrm{L} \text { sine } \mathrm{S}^{\circ} ; \\
\mathrm{V} \mathrm{~B} & =\mathrm{V} \mathrm{~S}-\left(\mathrm{Y}+\mathrm{V}^{\prime} \mathrm{L}-\mathrm{V}^{\prime} \mathrm{L} \text { versine } \mathrm{S}^{\circ}\right) ; \\
\tan \mathrm{C} & =\frac{\mathrm{V}^{\prime} \mathrm{B}}{\mathrm{VB}} \\
\mathrm{~V} \mathrm{~V}^{\prime} & =\frac{\mathrm{V} \mathrm{~B}}{\operatorname{cosine}} \text { if } \mathrm{C}=45^{\circ}-; \\
\mathrm{V} \mathrm{~V}^{\prime} & =\frac{\mathrm{V}^{\prime} \mathrm{B}}{\operatorname{sine} \mathrm{C}} \text { if } \mathrm{C}=45^{\circ}+.
\end{aligned}
$$



Problem 10

Problem 10. Given: The middle ordinate for a chord of length $a b$ for $R$ and $R^{\prime}$, to find the middle ordinate at the P C C. From the figure it is evident that $\mathrm{d}^{\prime} \mathrm{c}^{\prime}$ bisects $\mathrm{c} d$.

$$
\therefore e f=\frac{c f+d f}{2}
$$

Therefore, the middle ordinate at any P C C in the spiral equals one-half the sum of the middle ordinates for the radii on each side for the same chord.


Problem 11
Problem 11. Given: That portion of a spiral with equal chords $\mathrm{L}, \mathrm{L}^{\prime}$ and $\mathrm{L}^{\prime \prime}$ and angles $a-b, a$, and $a+b$, to find the middle ordinate at the center of the chord L in the length $\mathrm{D}^{\prime} \mathrm{C}^{\prime}$.

$$
\mathrm{CF}=\mathrm{C}^{\prime} \mathrm{A} \text { and } \mathrm{DF}=\mathrm{D}^{\prime} \mathrm{B}
$$

From the figure it is evident that $\mathrm{D}^{\prime} \mathrm{C}^{\prime}$ bisects C D.

$$
\therefore \mathrm{E} \mathrm{~F}=\frac{\mathrm{C} \mathrm{~F}+\mathrm{D} \mathrm{~F}}{2}
$$

Then $\mathrm{C}^{\prime} \mathrm{A}=1 / 2 \mathrm{~L} \tan 1 / 4 a+\mathrm{L}^{\prime}$ sine $\left(1 / 2 a+\frac{a+b}{2}\right)$;

$$
\mathrm{D}^{\prime} \mathrm{B}=1 / 2 \mathrm{~L} \tan 1 / 4 a+\mathrm{L}^{\prime \prime} \text { sine }\left(1 / 2 a+\frac{a-b}{2}\right)
$$

and since the sines of small angles are proportional to the angles,

$$
\frac{\mathrm{C} \mathrm{~F}+\mathrm{D} \mathrm{~F}}{2}=\mathrm{E} \mathrm{~F}=1 / 2 \mathrm{~L} \tan 1 / 4 a+\mathrm{L} \text { sine } a .
$$

But this last equation equals the middle ordinate in the length $A B$ for the radius of the central arc; and since the increment to the angle $b$ would be equal if $L^{\prime}$ and $L^{\prime \prime}$ were equal, the middle ordinate at the center of any arc of the spiral, for any length of chord, is equal to the middle ordinate of the radius of that are in the same length.

## Standard Spirals.

## The Pennsylvania Steel Co.

## Center Line Data.

## SPIRAL No. 2

| Rad. | Angle | X | Y | $\mathrm{S}^{\circ}$ | Versine | Sine |
| :---: | :---: | :---: | :---: | ---: | :---: | :---: |
| 300 | $0^{\circ}-30^{\prime}$ | 0.011 | 2.618 | $0^{\circ}-30^{\prime}$ | .00004 | .00873 |
| 150 | $1^{\circ}-00^{\prime}$ | 0.057 | 5.235 | $1^{\circ}-0^{\circ}$ | .00034 | .02618 |
| 100 | $1^{\circ}-30^{\prime}$ | 0.160 | 7.851 | $3^{\circ}-00^{\prime}$ | .00137 | .05234 |
| 75 | $2^{\circ}-00^{\prime}$ | 0.342 | 10.463 | $5^{\circ}-00^{\prime}$ | .00381 | .08716 |
| 60 | $2^{\circ}-30^{\prime}$ | 0.627 | 13.065 | $7^{\circ}-30^{\prime}$ | .00856 | .13053 |
| 50 | $3^{\circ}-00^{\prime}$ | 1.036 | 15.651 | $10^{\circ}-30^{\prime}$ | .01675 | .18224 |
| $421 / 2$ | $3^{\circ}-30^{\prime}$ | 1.587 | 18.187 | $14^{\circ}-00^{\prime}$ | .02970 | .24192 |
| $37 / 2$ | $4^{\circ}-00^{\prime}$ | 2.309 | 20.703 | $18^{\circ}-00^{\prime}$ | .04894 | .30902 |

## SWITCH EASEMENT S 2-75

| Rad. | Angle | X | Y | $\mathrm{S}^{\circ}$ | This Ease- <br> ment gives an |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | 75 | $7^{\circ}-50^{\prime}$ | 0.700 | 10.222 | $7^{\circ}-50^{\prime}$ |
| O G equal to |  |  |  |  |  |

SPIRAL No. $2^{1 ⁄ 2}$

| Rad. | Angle | X | Y | So | Versine | Sine |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 444 | $0^{\circ}-20^{\prime}$ | 0.007 | 2.583 | $0^{\circ}-20^{\prime}$ | . 00002 | . 00582 |
| 222 | $0^{\circ}-40^{\prime}$ | 0.038 | 5.166 | $1^{\circ}-00^{\prime}$ | 00015 | 01745 |
| 148 | $1^{\circ}-00^{\prime}$ | 0.105 | 7.748 | $2^{\circ}-00^{\prime}$ | . 00061 | 03490 |
| 111 | $1^{\circ}-20^{\prime}$ | 0.226 | 10.328 | $3{ }^{\circ}-20^{\prime}$ | . 00169 | 05814 |
| 89 | $1^{\circ}-40^{\prime}$ | 0.414 | 12.910 | $5^{\circ}-00^{\prime}$ | 00381 | . 08716 |
| 74 | $2^{\circ}-00^{\prime}$ | 0.684 | 15.478 | $7{ }^{\circ}-00^{\prime}$ | . 00745 | 12187 |
| $631 / 2$ | $2^{\circ}-20^{\prime}$ | 1.051 | 18.038 | $9^{\circ}-20^{\prime}$ | . 01324 | 16218 |
| $551 / 2$ | $2^{\circ}-40^{\prime}$ | 1.529 | 20.576 | $12^{\circ}-00^{\prime}$ | . 02185 | 20791 |
| 49 | $3^{\circ}-00^{\prime}$ | 2.128 | 23.070 | $15^{\circ}-00^{\prime}$ | . 03407 | 25882 |
| $441 / 2$ | $3^{\circ}-20^{\prime}$ | 2.870 | 25.550 | $18^{\circ}-20^{\prime}$ | . 05076 | . 31454 |
| $401 / 2$ | $3^{\circ}-40^{\prime}$ | 3.763 | 27.983 | $22^{\circ}-00^{\prime}$ | . 07282 | . 37461 |

## SWITCH EASEMENT S 2½-100

| Rad. | Angle | X | Y | S ${ }^{\circ}$ | Ease- |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1021/3 | $6^{\circ}-30^{\prime}$ | 0.658 | 11.584 | $6^{\circ}-30^{\prime}$ | O G equal to |
| $561 / 2$ | $5^{\circ}-30^{\prime}$ | 1.529 | 16.936 | $12^{\circ}-00^{\prime}$ | and a G S |
| 49 | $3^{\circ}-00^{\prime}$ | 2.128 | 19.430 | $15^{\circ}-00^{\prime}$ | 3.640 less tha |
| $441 / 2$ | $3^{\circ}-20^{\prime}$ | 2.870 | 21.910 | $18^{\circ}-20^{\prime}$ |  |
| $401 / 2$ | $3^{\circ}-40^{\prime}$ | 3.763 | 24.343 | $22^{\circ}-00^{\prime}$ | Spiral No. $2 \frac{1}{2}$. |

## SWITCH EASEMENT S 2½-200

| Rad. | Angle | x | Y | S ${ }^{\circ}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 200 | $4^{\circ}-00^{\prime}$ | 0.487 | 13.951 | $4^{\circ}-00^{\prime}$ | ment gives an |
| 129 | $1^{\circ}-00^{\prime}$ | 0.664 | 16.196 | $5^{\circ}-00^{\prime}$ | O G 0.250 |
| 74 | $2^{\circ}-00^{\prime}$ | 0.934 | 18.764 | $7{ }^{\circ}-00^{\prime}$ | greater and |
| $631 / 2$ | $2^{\circ}-20^{\prime}$ | 1.301 | 21.324 | $9^{\circ}-20^{\prime}$ | $\mathrm{G} \quad \mathrm{S} \quad 3.286$ |
| $551 / 2$ | $2^{\circ}-40^{\prime}$ | 1.779 | 23.862 | $12^{\circ}-00^{\prime}$ |  |
| 49 | $3^{\circ}-00^{\prime}$ $3^{\circ}-20^{\prime}$ | 2.378 | 26.356 | $15^{\circ}-00^{\prime}$ | greater than |
| $441 / 2$ $401 / 2$ | $3^{\circ}-20^{\prime}$ $3^{\circ}-40^{\prime}$ | 3.120 4.013 | 28.836 31.269 | $18^{\circ}-20^{\prime}$ $22^{\circ}-00^{\prime}$ | Spiral No. $2 \frac{1}{2}$. |

SPIRAL No. 3

| Rad. | Angle | X | Y | $\mathrm{S}^{\circ}$ | Versine | Sine |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 300 |  | 0.046 | 5.236 | $1^{\circ}-00^{\prime}$ | .00015 |  |
|  | $2^{\circ}-00^{\prime}$ | 0.229 | 10.468 | $3^{\circ}-00^{\prime}$ | .00137 | .01745 |
| 100 | $3^{\circ}-00^{\prime}$ | 0.639 | 15.688 | $6^{\circ}-00^{\prime}$ | .00548 | .10453 |
| 75 | $4^{\circ}-00^{\prime}$ | 1.368 | 20.871 | $10^{\circ}-00^{\prime}$ | .01519 | .17365 |
| 60 | $5^{\circ}-00^{\prime}$ | 2.501 | 25.982 | $15^{\circ}-00^{\prime}$ | .03407 | .25882 |
| 50 | $6^{\circ}-00^{\prime}$ | 4.118 | 30.959 | $21^{\circ}-00^{\prime}$ | .06642 | .35837 |
| 40 | $7^{\circ}-00^{\prime}$ | 6.143 | 35.403 | $28^{\circ}-00^{\prime}$ | .11705 | .46947 |

## SWITCH EASEMENT S 3-100

| Rad. | Angle | X | Y | S ${ }^{\circ}$ | e- |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1021/3 | $6^{\circ}-30^{\prime}$ | 0.658 | 11.584 | $6^{\circ}-30^{\prime}$ | ment gives an |
| 81 | $3^{\circ}-30^{\prime}$ | 1.368 | 16.480 | $10^{\circ}-00^{\prime}$ | and a G S |
| 60 | $5{ }^{\circ}-00^{\prime}$ | 2.501 | 21.591 | $15^{\circ}-00^{\prime}$ | 4.391 less than |
| 50 | $6^{\circ}-00^{\prime}$ | 4.118 | 26.568 | $21^{\circ}-00^{\prime}$ | Spiral No. 3. |
| 40 | $7^{\circ}-00^{\prime}$ | 6.143 | 31.012 | $28^{\circ}-00^{\prime}$ | Spiral No. 3. |

## SWITCH EASEMENT S 3-200

| Rad. | Angle | x | Y | $5^{\circ}$ | This Ease- |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 200 | $4^{\circ}-00^{\prime}$ | 0.487 | 13.951 | $4^{\circ}-00^{\prime}$ | ment gives an |
| 132 | $2^{\circ}-00^{\prime}$ | 0.889 | 18.541 | $6^{\circ}-00^{\prime}$ |  |
| 75 | $4^{\circ}-00^{\prime}$ | 1.618 | 23.724 | $10^{\circ}-00^{\prime}$ | Greater and a |
| 60 | $5^{\circ}-00^{\prime}$ | 2.751 | 28.835 | $15^{\circ}-00^{\prime}$ | greater than |
| 50 | $6^{\circ}-00^{\prime}$ | 4.368 | 33.812 | $21^{\circ}-00^{\prime}$ | Spiral No. 3. |
| 40 | $7^{\circ}-00^{\prime}$ | 6.393 | 38.256 | $28^{\circ}-00^{\prime}$ | Spiral No. 3. |

SPIRAL No. 4

| Rad. | Angle | X | Y | $\mathrm{S}^{\circ}$ | Versine | Sine |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 420 | $0^{\circ}-42^{\prime}$ | 0.031 | 5.131 | $0^{\circ}-42^{\prime}$ | .00007 | .01222 |
| 210 | $1^{\circ}-24^{\prime}$ | 0.157 | 10.261 | $2^{\circ}-06^{\prime}$ | .00067 | .03664 |
| 140 | $2^{\circ}-06^{\prime}$ | 0.439 | 15.384 | $4^{\circ}-12^{\prime}$ | .00269 | .07324 |
| 105 | $2^{\circ}-48^{\prime}$ | 0.939 | 20.490 | $7^{\circ}-00^{\prime}$ | .00745 | .12187 |
| 84 | $3^{\circ}-30^{\prime}$ | 1.720 | 25.561 | $10^{\circ}-30^{\prime}$ | .01675 | .18224 |
| 70 | $4^{\circ}-12^{\prime}$ | 2.839 | 30.567 | $14^{\circ}-42^{\prime}$ | .03273 | .25376 |
| 60 | $4^{\circ}-54^{\prime}$ | 4.352 | 35.469 | $19^{\circ}-36^{\prime}$ | .05794 | .33545 |

## SWITCH EASEMENT S 4-200

| Rad. | Angle | x | Y | So | This Easement gives an O G 0.178 greater and a G S equal to Spiral No. 4. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 200 | $4^{\circ}-00^{\prime}$ | 0.487 | 13.951 | $4^{\circ}-00{ }^{\prime}$ |  |
| 1251/2 | $3^{\circ}-00^{\prime}$ | 1.117 | 20.490 | $7^{\circ}-00^{\prime}$ |  |
| 84 | $3^{\circ}-30^{\prime}$ | 1.898 | 25.561 | $10^{\circ}-30^{\prime}$ |  |
| 70 60 | $4^{\circ}-12^{\prime}$ $4^{\circ}-54^{\prime}$ | 3.017 4.530 | 30.567 35.469 | $14^{\circ}-42^{\prime}$ $19^{\circ}-36^{\prime}$ |  |

## SPIRAL No. 5

| Rad. | Angle | X | Y | $\mathrm{S}^{\circ}$ | Versine | Sine |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 600 | $0^{\circ}-30^{\prime}$ | 0.023 | 5.236 | $0^{\circ}-30^{\prime}$ | .00004 |  |
| 300 | $1^{\circ}-00^{\prime}$ | 0.114 | 10.471 | $1^{\circ}-30^{\prime}$ | .00034 | .02678 |
| 200 | $1^{\circ}-30^{\prime}$ | 0.320 | 15.703 | $3^{\circ}-00^{\prime}$ | .00137 | .05618 |
| 150 | $2^{\circ}-00^{\prime}$ | 0.685 | 20.926 | $5^{\circ}-00^{\prime}$ | .00381 | .082346 |
| 120 | $2^{\circ}-30^{\prime}$ | 1.255 | 26.130 | $7^{\circ}-30^{\prime}$ | .00856 | .13053 |
| 100 | $3^{\circ}-00^{\prime}$ | 2.073 | 31.302 | $10^{\circ}-30^{\prime}$ | .01675 | .18224 |
| 85 | $3^{\circ}-30^{\prime}$ | 3.175 | 36.374 | $14^{\circ}-00^{\prime}$ | .02970 | .24192 |

## SWITCH EASEMENT S 5-200

| Rad. | Angle | X | Y | $S^{\circ}$ | This Ease- |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 200 | $4^{\circ}-00^{\prime}$ | 0.487 | 13.951 | $4^{\circ}-00^{\prime}$ | ment gives an |
| 144 | $1^{\circ}-00^{\prime}$ | 0.685 | 16.458 | $5^{\circ}-00^{\prime}$ | $\bigcirc \mathrm{G}$ equal to |
| 120 | $2^{\circ}-30^{\prime}$ | 1.255 | 21.662 | $7{ }^{7}-30^{\prime}$ | and 4.468 less than |
| 100 | $3^{\circ}-00^{\prime}$ | 2.073 | 26.834 | $10^{\circ}-30^{\prime}$ | 4.468 less than |
| 85 | $3^{\circ}-30^{\prime}$ | 3.175 | 31.906 | $14^{\circ}-00^{\prime}$ | Spiral No. 0. |

## SPIRAL No. 6

| Rad. | Angle | x | Y | So | Versine | Sine |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 900 | $0^{\circ}-20^{\prime}$ | 0.015 | 5.236 | $0^{\circ}-20^{\prime}$ | . 00002 | . 00582 |
| 450 | $0^{\circ}-40^{\prime}$ | 0.076 | 10.472 | $1^{\circ}-00^{\prime}$ | . 00015 | . 01745 |
| 300 | $1^{\circ}-00^{\prime}$ | 0.213 | 15.706 | $2^{\circ}-00^{\prime}$ | . 00061 | . 03490 |
| 225 | $1^{\circ}-20^{\prime}$ | 0.457 | 20.936 | $3^{\circ}-20^{\prime}$ | . 00169 | . 05814 |
| 180 | $1^{\circ}-40^{\prime}$ | 0.837 | 26.158 | $5^{\circ}-00^{\prime}$ | . 00381 | . 08716 |
| 150 | $2^{\circ}-00^{\prime}$ | 1.385 | 31.365 | $7^{\circ}-00^{\prime}$ | . 00745 | . 12187 |
| 128 | $2^{\circ}-20^{\prime}$ | 2.125 | 36.524 | $9^{\circ}-20^{\prime}$ | . 01324 | . 16218 |

SWITCH EASEMENT S 6-200

| Rad. | Angle | x | Y | So | This Ease ment gives an $O$ G equal to and a G S 7.770 less than Spiral No. 6. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 200 | $4^{\circ}-00^{\prime}$ | 0.487 | 13.951 | $4^{\circ}-00^{\prime}$ |  |
| 255 | $1^{\circ}-00^{\prime}$ | 0.837 | 18.388 | $5^{\circ}-00^{\prime}$ |  |
| 150 | $2^{\circ}-00^{\prime}$ | 1.385 | 23.595 | $7^{\circ}-00^{\prime}$ |  |
| 128 | $2^{\circ}-20^{\prime}$ | 2.125 | 28.754 | $9^{\circ}-20^{\prime}$ |  |

## SPIRAL No. 7

| Rad. | Angle | X | Y | $\mathrm{S}^{\circ}$ | Versine | Sine |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| 1260 | $0^{\circ}-15^{\prime}$ | 0.012 | 5.498 | $0^{\circ}-15^{\prime}$ | .00001 | .00436 |
| 630 | $0^{\circ}-30^{\prime}$ | 0.060 | 10.995 | $0^{\circ}-45^{\prime}$ | .00009 | .01309 |
| 420 | $0^{\circ}-45^{\prime}$ | 0.168 | 16.492 | $1^{\circ}-30^{\prime}$ | .00034 | .02618 |
| 315 | $1^{\circ}-00^{\prime}$ | 0.360 | 21.987 | $2^{\circ}-30^{\prime}$ | .00095 | .04362 |
| 252 | $1^{\circ}-15^{\prime}$ | 0.660 | 27.475 | $3^{\circ}-45^{\prime}$ | .00214 | .06540 |
| 210 | $1^{\circ}-30^{\prime}$ | 1.091 | 32.957 | $5^{\circ}-15^{\prime}$ | .00420 | .09150 |
| 180 | $1^{\circ}-45^{\prime}$ | 1.678 | 38.424 | $\gamma^{\circ}-00^{\prime}$ | .00745 | .12187 |
| 157 |  |  |  |  |  |  |

SPIRAL No. 8

| Rad. | Angle | X | Y | $\mathrm{S}^{\circ}$ | Versine | Sine |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1890 | $0^{\circ}-10^{\prime}$ | 0.008 | 5.498 | $0^{\circ}-10^{\prime}$ | .00000 | .00291 |
| 945 | $0^{\circ}-20^{\prime}$ | 0.040 | 10.996 | $0^{\circ}-30^{\prime}$ | .00004 | .00873 |
| 630 | $0^{\circ}-30^{\prime}$ | 0.112 | 16.493 | $1^{\circ}{ }^{\circ} 00^{\prime}$ | .00015 | .01745 |
| $4721 / 2$ | $0^{\circ}-40^{\prime}$ | 0.241 | 21.990 | $1^{\circ}-40^{\prime}$ | .00042 | .02908 |
| 378 | $0^{\circ}-50^{\prime}$ | 0.441 | 27.483 | $2^{\circ}-30^{\prime}$ | .00095 | .04362 |
| 315 | $1^{\circ}-00^{\prime}$ | 0.729 | 32.973 | $3^{\circ}-30^{\prime}$ | .00187 | .06105 |
| 270 | $1^{\circ}-10^{\prime}$ | 1.120 | 38.457 | $4^{\circ}-40^{\prime}$ | .00332 | .08136 |
| 236 |  |  |  |  |  |  |

## SPIRAL No. 9

| Rad. | Angle | x | y | S $^{\circ}$ | Versine | Sine |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2730 | $0^{\circ}-7^{\prime}$ | 0.006 | 5.559 | $0^{\circ}-7^{\prime}$ | .00000 | .00204 |
| 1365 | $0^{\circ}-14^{\prime}$ | 0.028 | 11.118 | $0^{\circ}-21^{\prime}$ | .00002 | .00611 |
| 910 | $0^{\circ}-21^{\prime}$ | 0.079 | 16.677 | $0^{\circ}-42^{\prime}$ | .00007 | .01222 |
| $6821 / 2$ | $0^{\circ}-28^{\prime}$ | 0.170 | 22.234 | $1^{\circ}{ }^{\circ}-10^{\prime}$ | .00021 | .02036 |
| 546 | $0^{\circ}-35^{\prime}$ | 0.311 | 27.791 | $1^{\circ}-45^{\prime}$ | .00047 | .03054 |
| 455 | $0^{\circ}-42^{\prime}$ | 0.515 | 33.346 | $2^{\circ}-27^{\prime}$ | .00091 | .04275 |
| 390 | $0^{\circ}-49^{\prime}$ | 0.792 | 38.899 | $3^{\circ}-16^{\prime}$ | .00162 | .05698 |
| 341 |  |  |  |  |  |  |

## SPIRAL No. 10

| Rad. | Angle | x | y | $\mathrm{S}^{\circ}$ | Versine | Sine |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3780 | $0^{\circ}-05^{\prime}$ |  | 0.004 | 5.498 | $0^{\circ}-05^{\prime}$ | .00000 |
| 1890 | $0^{\circ}-10^{\prime}$ | 0.020 | 10.996 | $0^{\circ}{ }^{\circ}-15^{\prime}$ | .00001 | .00145 |
| 1260 | $0^{\circ}-15^{\prime}$ | 0.056 | 16.493 | $0^{\circ}{ }^{\circ}-30^{\prime}$ | .00004 | .00876 |
| 945 | $0^{\circ}-20^{\prime}$ | 0.120 | 21.991 | $0^{\circ}-50^{\prime}$ | .00011 | .01454 |
| 756 | $0^{\circ}-25^{\prime}$ | 0.220 | 27.488 | $1^{\circ}-15^{\prime}$ | .00024 | .02181 |
| 630 | $0^{\circ}-30^{\prime}$ | 0.364 | 32.983 | $1^{\circ}-45^{\prime}$ | .00047 | .03054 |
| 540 | $0^{\circ}-35^{\prime}$ | 0.560 | 38.478 | $2^{\circ}-20^{\prime}$ | .00083 | .04071 |
| 472 |  |  |  |  |  |  |

## SPIRAL No. 11

| Rad. | Angle | X | Y | $\mathrm{S}^{\circ}$ | Versine | Sine |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 5250 | $0^{\circ}-04^{\prime}$ | .0035 | 6.109 | $0^{\circ}-04^{\prime}$ | .00000 | .00116 |
| 2625 | $0^{\circ}-08^{\prime}$ | .0178 | 12.217 | $0^{\circ}-12^{\prime}$ | .00001 | .00349 |
| 1750 | $0^{\circ}-12^{\prime}$ | .0498 | 18.326 | $0^{\circ}{ }^{\circ}-24^{\prime}$ | .00002 | .00698 |
| $13121 / 2$ | $0^{\circ}-16^{\prime}$ | .1066 | 24.434 | $0^{\circ}-40^{\prime}$ | .00007 | .01164 |
| 1050 | $0^{\circ}-20^{\prime}$ | .1955 | 30.542 | $1^{\circ}-00^{\prime}$ | .00015 | .01745 |
| 875 | $0^{\circ}-24^{\prime}$ | .3234 | 36.649 | $1^{\circ}-24^{\prime}$ | .00030 | .02443 |
| 750 | $0^{\circ}-28^{\prime}$ | .4975 | 42.756 | $1^{\circ}-52^{\prime}$ | .00053 | .03257 |
| 656 |  |  |  |  |  |  |

## SPIRAL No. 12

| Rad. | Angle | X | Y | So | Versine | Sine |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7140 | $0^{\circ}-03^{\prime}$ | . 0027 | 6.231 | $0^{\circ}-03^{\prime}$ | . 00000 | . 00087 |
| 3570 | $0^{\circ}-06^{\prime}$ | . 0136 | 12.462 | $0^{\circ}-09^{\prime}$ | . 00000 | . 00262 |
| 2380 | $0^{\circ}-09^{\prime}$ | . 0381 | 18.692 | $0^{\circ}-18^{\prime}$ | . 00001 | . 00524 |
| 1785 | $0^{\circ}-12^{\prime}$ | . 0816 | 24.923 | $0^{\circ}-30^{\prime}$ | . 00004 | . 00873 |
| 1428 | $0^{\circ}-15^{\prime}$ | . 1495 | 31.153 | $0^{\circ}-45^{\prime}$ | . 00009 | . 01309 |
| 1190 | $0^{\circ}-18^{\prime}$ | . 2474 | 37.384 | $1^{\circ}-03^{\prime}$ | . 00017 | . 01832 |
| 1020 892 | $0^{\circ}-21^{\prime}$ | . 3806 | 43.613 | $1^{\circ}-24^{\prime}$ | . 00030 | .02443 |

Tables giving elements of SPIRALS
for
Inner Gage Line Lengths of Rails and

Tie Rod Spacing for

> Various Gages.


|  | ${ }_{\text {Cont. }}^{\text {Cent. }}$ | Angle | Inner Rail |  | so | ${ }_{\substack{\text { Length } \\ \text { Outer }}}^{\text {L }}$ | $\underbrace{\substack{\text { a }}}_{\substack{\text { Length } \\ \text { Inner }}}$ | $\underset{\substack{\text { Correc. } \\ \text { tion Rair } \\ \text { T Rail }}}{\substack{\text { and }}}$ | This Easement gives an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |
|  | 75 | $7^{\circ}-50^{\prime}$ | . 678 | 9.901 | $7{ }^{\circ}-50^{\prime}$ | 10.576 | 9.932 | . 012 | O G equal to |
| 6 | 451/3 | $2^{\circ}-40^{\prime}$ | . 997 | 11.876 | $10^{\circ}-30^{\prime}$ | 12.795 | 11.933 | . 016 | 3.346 less than |
| 7 | 421/2 | $3^{\circ}-30^{\prime}$ | 1.517 | 14.272 | $14^{\circ}-00^{\prime}$ | 15.535 | 14.385 | . 022 | Spiral No. 2. |
| 8 | $371 / 2$ | $4^{\circ}-00^{\prime}$ | 2.194 | 16.630 | $18^{\circ}-00^{\prime}$ | 18.318 | 16.838 | . 028 |  |


| ${ }_{\substack{\text { Point } \\ \text { No. }}}^{\text {d }}$ | $\xrightarrow{\text { Cent. }}$ Rad. | Angle | Inner Rail |  |  | Versin |  |  | ${ }_{\text {Length }}^{\text {Outer }}$ |  | Length | $\begin{gathered} \text { Correcor } \\ \text { tion for } \\ \text { T Ratid } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 1 \\ & \frac{1}{2} \\ & \frac{3}{3} \\ & 4 \\ & \hline 6 \\ & 6 \\ & 7 \\ & \hline \\ & 10 \\ & 10 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{array}{ll} \hline 2.569 \\ \hline \end{array}$ | 0.00 <br> 0.000 <br> 0.003 <br> 0.008 <br> 0.008 <br> 0.01 <br> 0.015 <br> 0.015 <br> 0.012 <br> 0.025 <br> 0.025 <br> 0.025 |
| TIE ROD DISTANCES FROM P. S. |  |  |  |  |  |  |  |  |  |  |  |  |
| $\frac{\text { Inner }}{\text { Rai1 }}$ | ${ }_{\text {Outer }}^{\text {Rait }}$ | Inner | ${ }_{\text {Outer }}^{\substack{\text { Outid }}}$ | Inner | $\underset{\substack{\text { Outer } \\ \text { Rail }}}{\text { are }}$ | ${ }_{\text {Inner }}^{\text {Rail }}$ | Outer Rail |  |  | Outer Rail | Inner | ${ }_{\text {Outer }}^{\text {Ouil }}$ |
| $\begin{gathered} 1.00 \\ \text { and } \\ 2: 90 \\ 4.909 \end{gathered}$ | $\begin{aligned} & 1.00 \\ & .0 .0 \\ & 0.00 \\ & 5.00 \end{aligned}$ |  | $\begin{aligned} & 6.05 \\ & \hline 6.07 \\ & \hline, 0.01 \\ & 10.11 \end{aligned}$ | 10.85 11.82 18.76 18.73 18.72 |  |  |  |  |  |  | $\begin{aligned} & 259.98 \\ & 27: 128 \end{aligned}$ | cois |


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|  | is |  <br> © |  | is |  |
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| Ei | $\begin{aligned} & \stackrel{.}{n} \\ & \stackrel{H}{0} \\ & \stackrel{5}{5} \end{aligned}$ |  |  |  |  <br>  |
| $\begin{aligned} & \text { サ } \\ & \text { 区iv } \\ & \text { U } \\ & \text { U } \end{aligned}$ |  | \％080\％\％ |  | 言氟品 |  <br>  |
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SWITCH EASEMENT S 3-100



| $\xrightarrow{\text { Point }}$ No. | $\underset{\substack{\text { Cent. } \\ \text { Rad. }}}{\text { a }}$ | Angle | Inner Rail |  | so | ${ }_{\text {L }}^{\text {Length }}$ Outer | ${ }_{\substack{\text { Length } \\ \text { Inner }}}^{\substack{\text { den }}}$ | $\begin{gathered} \text { Correc } \\ \text { tion } \\ \text { T Raid } \\ \text { Raid } \end{gathered}$ | This Ease- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.481 | $13.787^{\circ}$ | $4^{\circ}-00^{\prime}$ | 14.127 | 13.799 | . 006 | ment gives an |
| 4 | 1251/2 | $3^{\circ}-00^{\prime}$ | 1.099 | 20.203 | $7{ }^{\circ}-00^{\prime}$ | 20.822 | 20.246 | 011 | greater and |
| 5 | 84 | $3^{\circ}-30^{\prime}$ | 1.859 | 25.132 | $10^{\circ}-30^{\prime}$ | 26.096 | 25.234 | . 016 | G S equal |
| 6 | 70 | $4^{\circ}-12^{\prime}$ | 2.940 | 29.970 | 14 ${ }^{\circ}-42^{\prime}$ | 31.400 | 30.192 | . 023 | Spiral No. 4. |
| 7 | 60 | $4^{\circ}-54^{\prime}$ | 4.394 | 34.679 | $19^{\circ}-36^{\prime}$ | 36.733 | 35.123 | . 031 |  |


SWITCH EASEMENT

| $\xrightarrow{\text { Point }}$ No. | ${ }_{\substack{\text { cent. } \\ \text { Rad. }}}$ | Angle | Inner Rail |  | so | $\underset{\substack{\text { Length } \\ \text { Outer }}}{\text { den }}$ |  | $\begin{gathered} \text { Correc. } \\ \text { Tion } \\ \hline \text { Tor } \\ \hline \text { Rair } \end{gathered}$ | This Ease- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.481 | 13.787 | $4^{\circ}-00^{\circ}$ | 14.127 | 13.799 | . 006 | ment gives an |
| 4 | 144 | $1^{\circ}-00^{\prime}$ | 0.676 | 16.253 | $5{ }^{\circ}-00$ | 16.681 | 16.271 | . 008 | and a G S |
| 5 | 120 | $2^{\circ}-30^{\prime}$ | 1.235 | 21.355 | $7^{\circ}-30^{\prime}$ | 22.020 | 21.404 | . 012 | 4.468 less than |
| 6 | 100 | $3^{\circ}-00^{\prime}$ | 2.034 | 26.405 | $10^{\circ}-30^{\prime}$ | 27.379 | 26.517 | . 016 | Spiral No. 5 |
| 7 | 85 | $3^{\circ}-30^{\prime}$ | 3.105 | 31.337 | $14^{\circ}-00^{\prime}$ | 32.715 | 31.565 | . 022 |  |



| $\xrightarrow{\text { Point }}$ No. | Cent. | Angle | Inner Rail |  | so | $\underset{\substack{\text { Length } \\ \text { Outer }}}{ }$ | Length | $\begin{gathered} \text { Correcor } \\ \text { citor } \\ \hline \text { Ton Rair } \end{gathered}$ | This Ease ment gives an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.481 | 13.787 | $4^{\circ}-00^{\prime}$ | 14.127 | 13.799 | . 006 | O G equal |
| 5 | 255 | $1^{\circ}-00^{\prime}$ | 0.828 | 18.183 | $5^{\circ}-00^{\prime}$ | 18.618 | 18.208 | . 008 | and a G S |
| 6 | 150 | $2^{\circ}-00^{\prime}$ | 1.367 | 23.308 | $7^{\circ}-00^{\prime}$ | 23.937 | 23.361 | . 011 | 7.7701ess than Spiral No. 6. |
| 7 | 128 | $2^{\circ}-20^{\prime}$ | 2.094 | 28.372 | $9^{\circ}-20^{\prime}$ | 29.245 | 28.479 | . 015 |  |


SWITCH EASEMENT S 2-75. GAGE, 5 FT.

| $\xrightarrow{\text { Point }}$ No. | ${ }_{\substack{\text { cent } \\ \text { Rast }}}^{\text {cen }}$ | Angle | Inner Rail |  | so | $\xrightarrow{\text { Iongth }}$ |  |  | $\begin{gathered} \text { This Ease- } \\ \text { ment gives an } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | v |  |  |  |  |  |
|  | ${ }^{75}$ | $7^{\circ}-50$ | 677 | 9.881 | $7^{\circ}-50^{\circ}$ | 10.596 | 9.912 | . 012 | $\bigcirc \mathrm{O}$ equal to |
| 6 | 451/3 | $2^{\circ}-40^{\prime}$ | . 994 | 11.849 | $10^{\circ}-30^{\circ}$ | 12.823 | 11.906 | . 016 | and a G S 3.36 lessthan |
| 7 | 421/2 | $3^{\circ}-30^{\prime}$ | 1.513 | 14.238 | $14^{\circ}-00$ | 15.571 | 14.349 | 023 | Spiral No. 2. |
| 8 | 371/2 | $4{ }^{-00}$ | 2.187 | 16.584 | 18-00 | 18.363 | 16.793 | 028 |  |

SPIRAL

| Point No． | Cent． Rad． | Angle | Inner Rail |  | $\mathbf{S}^{\circ}$ | Versine | Sine | Length Outer | Length Inner | Correc－ tion for T Rail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | X | Y |  |  |  |  |  |  |
| 1 | 444 | $0^{\circ}-20^{\prime}$ | ． 007 | 2.568 | $0^{\circ}-20^{\prime}$ | ． 00002 | ． 00582 | 2.598 | 2.568 | 0.000 |
| 2 | 228 | $0^{\circ}-40^{\prime}$ | ． 038 | 5.122 | $1^{\circ}-00^{\prime}$ | ． 00015 | ． 01745 | 5.210 | 5.122 | 0.002 |
| 3 | 148 | $1^{10}-00^{\prime}$ | 0.103 | 7.661 | $2^{\circ}-00^{\prime}$ | ． 00061 | ． 03490 | 7.836 | 7.662 | 0.008 |
| 4 | 111 | $1^{\circ}-20^{\prime}$ | 0.222 | 10.183 | $30-20{ }^{\prime}$ | ． 00169 | ． 05814 | 10.477 | 10.187 | 0.005 |
| 5 | 89 | $1^{\circ}-40^{\prime}$ | 0.404 | 12.692 | $5^{\circ}-00^{\prime}$ | ． 00381 | ． 08716 | 13.139 | 12.703 | 0.008 |
| 6 | 74 | $2^{\circ}-00^{\prime}$ | 0.665 | 15.173 | $7^{\circ}-00^{\prime}$ | ． 00745 | ． 12187 | 15.809 | 15.199 | 0.011 |
| 7 | $631 / 2$ | $2^{\circ}-20^{\prime}$ | 1.018 | 17.633 | 9${ }^{9}-20^{\prime}$ | ． 01324 | ． 16218 | 18.497 | 17.683 | 0.015 |
| 8 | $55^{1 / 2}$ | $3^{\circ}-40^{\prime}$ | 1.474 | 20.056 | $12^{\circ}-00^{\prime}$ | ． 02185 | ． 20791 | 21.197 | 20.149 | 0.019 |
| 9 10 | 49 | $3^{\circ}-00^{\prime}$ $3^{\circ}-20^{\prime}$ | 2.043 2.743 | 22.423 24.764 | $15^{\circ}-00^{\prime}$ $180.20^{\prime}$ | ． 03407 | ． 25882 | 23.898 | 22.585 | 0.024 |
| 11 | $441 / 2$ $401 / 2$ | $3 \circ-20^{\prime}$ $30-40^{\prime}$ | 2.743 3.581 | 24.764 27.046 | $18^{\circ}-20^{\prime}$ $22^{\circ}-00^{\prime}$ | ． 05076 | ． 31454 | 26.628 | 25.028 | 0.029 |
|  | 40／2 | $3-40$ | 3.581 | 27.046 | $22^{\circ}-00^{\prime}$ | ． 07282 | ． 37461 | 29.380 | 27.460 | 0.035 |

## TIE ROD DISTANCES FROM P．S．

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|  | 유귱 <br> ลั® |
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SWITCH EASEMENT S 2½-100.


|  | Cent. <br> Rad. | Angle | Inner Rail |  | so | Versine | Sine |  | ${ }_{\substack{\text { Length } \\ \text { Outer }}}$ |  | Length |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | Y |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 0 \\ & \frac{1}{6} \\ & 6 \\ & 7 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & .002 \\ & .005 \\ & .009 \\ & .0 .096 \\ & .0 .035 \\ & .034 \\ & .044 \end{aligned}$ |
| TIE ROD DISTANCES FROM P. S. |  |  |  |  |  |  |  |  |  |  |  |  |
| ${ }_{\text {Inner }}^{\text {Rail }}$ | $\xrightarrow{\text { Outer }}$ Rail | ${ }_{\text {Inner }}^{\text {Inail }}$ | $\begin{array}{c}\text { Outer } \\ \text { Rail }\end{array}$ | ${ }_{\substack{\text { Inner } \\ \text { Raii }}}$ | $\xrightarrow{\substack{\text { unter } \\ \text { Rail }}}$ | $\xrightarrow{\text { Inner }}$ Rail | ( $\begin{gathered}\text { Outer } \\ \text { Rail }\end{gathered}$ | ${ }_{\text {Inn }}^{\text {Ina }}$ |  | Outer | Inner <br> Rail | Outer <br> Rail |
|  |  |  | $\begin{array}{\|c} 7.07 \\ .09 \\ \text { o.11 } \\ \text { 10.12 } \\ 12.17 \\ 12.17 \end{array}$ | $\begin{aligned} & 12.81 \\ & \hline 1.88 \\ & 14.76 \\ & 11.78 \\ & 16.70 \\ & 17.68 \\ & 17.68 \end{aligned}$ | $\begin{aligned} & 13.19 \\ & 14.92 \\ & 15.24 \\ & 17.20 \\ & 17.30 \\ & 18.34 \end{aligned}$ |  |  |  |  |  |  |  |


| ${ }_{\substack{\text { Point } \\ \text { No. }}}^{\text {Pr }}$ | Cent. <br> Rad. | An | Inner Rail |  | so | Length <br> Outer <br> Oter | ${ }_{\substack{\text { Length } \\ \text { Inner }}}^{\text {cter }}$ |  | This Easement gives an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |
|  | 102 | $6^{\circ}$ | 0.642 | 11.301 | $6^{\circ}-30^{\prime}$ | 11.893 | 11.325 | . 010 | O G equal to |
| 4 | ${ }_{8}^{81}$ |  | ${ }^{1.330}$ | ${ }_{26}^{16.046}$ | ${ }^{10^{\circ}-00}$ | ${ }^{16.993}$ | ${ }^{16.121}$ | . 016 | and a G S |
| 5 | 60 <br> 50 | 5000 | 2.416 | ${ }^{20.944}$ | $15^{10^{\circ}}$ | ${ }_{\text {2. }}^{2.447}$ | ${ }^{21.139}$ | . 024 | 4.391 les |
| ${ }_{7}^{6}$ |  | $7^{6}{ }^{\circ}-000^{\circ}$ | ${ }^{3} .850$ | ${ }_{29}^{25.638}$ |  | 27.945 33.138 | ${ }_{30}^{26.113}$ | . 044 | Spiral No. 3. |
|  |  | IT | EA | M | T S | 200. | GA | 5 |  |
| Point |  | Angle |  | Rail |  | Length | ¢ng |  | This |
|  |  |  | x | Y |  |  | Innes | TR | ent gives an |
|  | 200 |  | 0.481 | 13.777 | $4^{\circ}-00$ | 14.138 |  | . 006 | O G 0.250 |
| 3 <br> 4 | ${ }_{75}^{132}$ |  | 0.875 1.580 | lis ${ }_{23}^{18.280}$ |  | ${ }_{24.242}^{18.832}$ | ${ }^{18.388}{ }_{23}^{1830}$ | . 016 | greater and a G S 2.853 |
| 5 | 60 | $5^{\circ}{ }^{\circ}-00^{\prime}$ | ${ }_{2} .666$ | ${ }_{28.188}$ | ${ }^{15}{ }^{\circ}-00^{\prime}$ | ${ }_{29.696}^{29}$ | ${ }_{28.388}^{288}$ | . 024 | greater than |
| ${ }_{7}^{6}$ | 50 40 | $6^{6}{ }^{\circ}-000^{\prime}$ | ${ }_{6}^{4.202}$ | ${ }^{33.916}$ | ${ }^{211^{\circ}-00^{\prime}}$ | 35.198 | 33.362 | . 033 | Spiral No. 3. |
|  | 40 | $7^{\circ}-00$ | 6.100 | 37.082 | $28^{\circ}-00^{\prime}$ | 40.387 | 37.943 | . 044 |  |


SWITCH EASEMENT S 4-200. GAGE, 5 FT.

| $\begin{aligned} & \text { Point } \\ & \text { No. } \end{aligned}$ | Cent.Rad. | Angle | Inner Rail |  | So | $\underset{\substack{\text { Length } \\ \text { Outer }}}{\substack{\text { nen }}}$ | $\begin{aligned} & \text { Length } \\ & \text { Inner } \end{aligned}$ | Correc- <br> T Rail | This Easement gives an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | Y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.481 | 13.777 | $4^{\circ}-00^{\prime}$ | 14.138 | 13.788 | . 006 | O G 0.178 |
| 4 | 1251/2 | $3^{\circ}-00^{\prime}$ | 1.098 | 20.185 | $7{ }^{\circ}-00^{\prime}$ | 20.839 | 20.229 | . 011 | greater an |
| 5 | 84 | $3^{\circ}-30^{\prime}$ | 1.856 | 25.105 | $10^{\circ}-30^{\prime}$ | 26.123 | 25.207 | . 016 | to Spiral No. |
| 6 | 70 | $4^{\circ}-12^{\prime}$ | 2.935 | 29.933 | $14^{\circ}-42^{\prime}$ | 31.437 | 30.155 | . 023 |  |
| 7 | 60 | $4^{\circ}-54^{\prime}$ | 4.385 | 34.630 | $19^{\circ}-36^{\prime}$ | 36.783 | 35.073 | . 031 |  |


SWITCH EASEMENT S 5-200. GAGE, 5 FT.

| $\begin{gathered} \text { Point } \\ \text { No. } \end{gathered}$ | $\begin{aligned} & \text { Cent. } \\ & \text { Rad. } \end{aligned}$ | Angle | Inner Rail |  | So | $\begin{aligned} & \text { Length } \\ & \text { Outer } \end{aligned}$ | $\underset{\substack{\text { Length } \\ \text { Inner }}}{ }$ | $\begin{aligned} & \text { Correc- } \\ & \text { tion for } \\ & \text { T Rail } \end{aligned}$ | This Ease- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | Y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.481 | 13.777 | $4^{\circ}-00^{\prime}$ | 14.138 | 13.788 | . 006 | O G equal to |
| 4 | 144 | $1^{\circ}-00^{\prime}$ | 0.675 | 16.240 | $5{ }^{\circ}-00$ | 16.694 | 16.258 | . 008 | and a G S |
| 5 | 120 | $2{ }^{\circ}-30^{\prime}$ | 1.234 | 21.336 | $7{ }^{\circ}-30^{\prime}$ | 22.039 | 21.385 | . 012 |  |
| 6 | 100 | $3^{\circ}-00^{\prime}$ | 2.031 | 26.378 | $10^{\circ}-30^{\prime}$ | 27.406 | 26.490 | . 016 |  |
| 7 | 85 | $3^{\circ}-30^{\prime}$ | 3.101 | 31.301 | $14^{\circ}-00^{\prime}$ | 32.751 | 31.529 | . 022 |  |



|  | $\underset{\text { Cent. }}{\text { Cond }}$ | Angle | Inner Rail |  | so | ${ }_{\substack{\text { Length } \\ \text { Outer }}}^{\text {Len }}$ | Length | $\begin{array}{\|c} \text { Correc- } \\ \text { tion } \\ \text { tion } \\ \text { Rair } \end{array}$ | This Easement gives an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.481 | 13.777 | $4^{\circ}-00^{\prime}$ | 14.138 | 13.788 | . 006 | $O G$ equal |
| 5 | 255 | $1^{\circ}-00^{\prime}$ | 0.828 | 18.170 | $5^{\circ}-00^{\prime}$ | 18.631 | 18.195 | . 008 | 7.770 less tha |
| 6 | 150 | $2^{\circ}-00^{\prime}$ | 1.366 | 23.290 | $7^{\circ}-00^{\prime}$ | 23.954 | 23.344 | . 011 | Spiral No. 6. |
| 7 | 128 | $2^{\circ}-20^{\prime}$ | 2.092 | 28.349 | $9^{\circ}-20^{\prime}$ | 29.269 | 28.455 | . 015 |  |



| $\xrightarrow[\substack{\text { Point } \\ \text { No. }}]{\text { coser }}$ | ${ }_{\text {Cont }}^{\text {Cent. }}$ Rad. | Angle | Inner Rail |  | so | $\underbrace{}_{\substack{\text { Length } \\ \text { Outer }}}$ | ${ }_{\substack{\text { Length } \\ \text { Inner }}}^{\substack{\text { der }}}$ | $\begin{gathered} \text { Correc } \\ \text { Cor } \\ \text { Ton } \\ \text { Taid } \end{gathered}$ | This Easement gives an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |
|  | 75 | $7{ }^{\circ}-50^{\prime}$ | . 676 | 9.867 | $7^{\circ}-50^{\prime}$ | 10.610 | 9.898 | . 012 | O G equal to |
| 6 | 451/3 | $2^{\circ}-40^{\prime}$ | . 992 | 11.830 | $10^{\circ}-30^{\prime}$ | 12.841 | 11.887 | . 016 | 3.346 less than |
| 7 | 421/2 | $3^{\circ}-30^{\prime}$ | 1.510 | 14.211 | $14^{\circ}-00^{\prime}$ | 15.596 | 14.324 | . 022 | Spiral No. 2. |
| 8 | $371 / 2$ | $4^{\circ}-00^{\prime}$ | 2.182 | 16.552 | $18^{\circ}-00^{\prime}$ | 18.396 | 16.760 | . 028 |  |


|  | $\underset{\substack{\text { Cent. } \\ \text { Rad. }}}{\text { cher }}$ | Angle | Inner Rail |  | so | Versine | Sin | Length |  | ${ }_{\text {L }}^{\substack{\text { Length } \\ \text { Iner }}}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | Y |  |  |  |  |  |  |  |
| 1 <br> $\frac{1}{2}$ <br> 8 <br> 4 <br> $\frac{4}{6}$ <br> $\frac{7}{7}$ <br> 8 <br> 10 <br> 10 <br> 10 |  |  |  |  |  |  |  |  |  |  | 0.000 <br> 0.003 <br> 0.003 <br> 0.005 <br> 0.001 <br> 0.015 <br> 0.015 <br> 0.019 <br> 0.024 <br> 0.029 <br> 0.025 <br> 0.035 |
| TIE ROD DISTANCES FROM P. S. |  |  |  |  |  |  |  |  |  |  |  |
| ${ }_{\substack{\text { Inner } \\ \text { Rail }}}^{\text {In }}$ | ${ }_{\text {Onter }}^{\substack{\text { Outer } \\ \text { Rail }}}$ | ${ }_{\text {Inner }}^{\text {Rail }}$ | ${ }_{\substack{\text { Outer } \\ \text { Rail }}}^{\text {den }}$ | ${ }_{\text {Inner }}^{\text {Rail }}$ | $\underset{\substack{\text { Outer } \\ \text { Rail }}}{\text { ar }}$ | ${ }_{\text {Rail }}^{\text {Inner }}$ | (outer | ${ }_{\text {Inner }}$ | er $\begin{aligned} & \text { Outer } \\ & \text { Rail } \\ & \text { Rail }\end{aligned}$ | ${ }_{\substack{\text { Inner } \\ \text { Rail }}}^{\text {arem }}$ | ${ }_{\substack{\text { Outer } \\ \text { Rail }}}$ |
| $\begin{aligned} & 1.99 \\ & \begin{array}{l} 1: 99 \\ 4.929 \\ 4.96 \end{array} \end{aligned}$ |  |  |  | $\begin{aligned} & 10.88 \\ & 11.80 \\ & 12.80 \\ & 18.78 \\ & 14.70 \end{aligned}$ | $\begin{aligned} & 11.120 \\ & 1292020 \\ & 15.250 \\ & 15.250 \end{aligned}$ | $\begin{gathered} 15.66 \\ 10.68 \\ \text { and } \\ 19.49 \end{gathered}$ |  |  |  | $\begin{aligned} & 25.16 \\ & \hline 20: 109 \end{aligned}$ |  |

SWITCH EASEMENT S 2½-100.



GAGE. 5 FT. $2^{1 ⁄ 2}$ IN.

| Point | ${ }_{\substack{\text { cont } \\ \text { Rad }}}$ | Anglo | Imper Rail |  | so | $\xrightarrow{\text { Longtr }}$ Onter |  |  | This Ease- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x |  |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.481 | 13.769 | $4^{8}-00^{\prime}$ | 14.145 | 13.781 | . 008 | ment gives an <br> O G 0.178 |
| 4 | 1251/2 | $3^{3}-00^{\circ}$ | 1.0 | 20.173 | $r^{\circ}-00$ | 20.852 | 20.216 | . 011 | grea |
| 5 | 84 | ${ }^{3}-30^{\circ}$ | 1. | 25.086 | 10 | 26.142 | 25.188 | . 016 | Spira |
| 6 | 70 | $4^{0}-12^{\prime}$ | 2.932 | 29.908 | 14-42 ${ }^{2}$ | 31.464 | 30.128 | . 023 | Spiral No |
|  | 60 | 40-54' | 4.379 | 34.595 | 19 -36 ${ }^{\circ}$ | 36.819 | 35.037 | . 031 |  |


SWITCH EASEMENT S $5-200$. GAGE. 5 FT. 2 $2 / 2$ IN.

| Point No. | Cent. Rad. | Angle | Inner Rail |  | $S^{\circ}$ | Length Outer | Length Inner | Correction for T Rail | This Easement gives an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | X | Y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.481 | 13.769 | $4^{\circ}-00^{\prime}$ | 14.145 | 13.781 | . 006 | O G equal |
| 4 | 144 | $11^{\circ}-00^{\prime}$ | 0.675 | 16.231 | $5^{\circ}-00^{\prime}$ | 16.703 | 16.249 | . 008 | and a G |
| 5 | 120 | $2^{\circ}-30^{\prime}$ | 1.233 | 21.322 | $7{ }^{\circ}-30^{\prime}$ | 22.053 | 21.371 | . 012 | 4.468 less than |
| 6 | 100 | $3^{\circ}-00^{\prime}$ | 2.029 | 26.360 | $10^{\circ}-30^{\prime}$ | 27.425 | 26.471 | . 016 |  |
| 7 | 85 | $3^{\circ}-30^{\prime}$ | 3.098 | 31.276 | $14^{\circ}-00^{\prime}$ | 32.776 | 31.504 | . 022 |  |


GAGE. 5 FT. $21 / 2 \mathrm{IN}$.

| Point No. | Cent. Rad. | Angle | Inner Rail |  | S ${ }^{\circ}$ | Length Outer | Length Inner | Correction for T Rail | This Easement gives an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | X | Y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.481 | 13.769 | $4^{\circ}-00^{\prime}$ | 14.145 | 13.781 | . 006 | G equal to |
| 5 | 255 | $1^{\circ}-00^{\prime}$ | 0.827 | 18.161 | $5^{\circ}-00^{\prime}$ | 18.640 | 18.186 | . 008 | 7.770 less than |
| 6 | 150 | $2^{\circ}-00^{\prime}$ | 1.366 | 23.278 | $7^{\circ}-00^{\prime}$ | 23.967 | 23.331 | . 011 | Spiral No. 6. |
| 7 | 128 | $2^{\circ}-20^{\prime}$ | 2.091 | 28.332 | $9^{\circ}-20^{\prime}$ | 29.286 | 28.438 | . 015 |  |


SWITCH EASEMENT S 2-75.

| PointNo. | Cent.Rad. | Angle | Inner Rail |  | So | $\begin{aligned} & \text { Length } \\ & \text { Outer } \end{aligned}$ | $\begin{aligned} & \text { Length } \\ & \text { Inner } \end{aligned}$ | $\begin{aligned} & \text { Correc- } \\ & \text { tion for } \\ & \text { T Rair } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | Y |  |  |  |  |  |
|  | 75 | $7{ }^{\circ}-50^{\prime}$ | . 675 | 9.856 | $7{ }^{\circ}-50^{\prime}$ | 10.621 | 9.887 | . 012 | G equal to |
| 6 | 451/3 | $2{ }^{\circ}-40^{\prime}$ | . 991 | 11.815 | $10^{\circ}-30^{\prime}$ | 12.857 | 11.871 | . 016 |  |
| 7 | 421/2 | $3^{\circ}-30^{\prime}$ | 1.507 | 14.191 | $14^{\circ}-00^{\prime}$ | 15.617 | 14.303 | . 022 | Spiral No. 2. |
| 8 | $371 / 2$ | $4^{\circ}-00^{\prime}$ | 2.177 | 16.526 | $18^{\circ}-00^{\prime}$ | 18.422 | 16.734 | . 028 |  |



| SWTTCE EASEMENT |  |  |  |  | $21 / 2-100$ |  | AGE, 5 FT |  | $41 / 2$ N. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Point No. | Cent. <br> Rad. | Angle | Inner Rail |  | $\mathrm{S}^{\circ}$ | Length Outer | Length Inner | Correction for T Rail | This Easement gives an O G equal to and a G S 3.640 less than Spiral No. $21 / 2$. |
|  |  |  | X | Y |  |  |  |  |  |
| $\begin{array}{r} 8 \\ 9 \\ 10 \\ 11 \end{array}$ | 1021/3 | $6^{\circ}-30^{\prime}$ | 0.641 | 11.280 | $6^{\circ}-30^{\prime}$ | 11.914 | 11.304 | . 010 |  |
|  | $561 / 2$ | $5^{\circ}-30^{\prime}$ | 1.470 | 16.377 | $12^{\circ}-00^{\prime}$ | 17.596 | 16.470 | . 019 |  |
|  | 49 | $3^{\circ}-00^{\prime}$ | 2.036 | 18.734 | $15^{\circ}-00^{\prime}$ | 20.303 | 18.895 | . 024 |  |
|  | $441 / 2$ | $3^{\circ}-20^{\prime}$ | 2.734 | 21.065 | $18^{\circ}-20^{\prime}$ | 23.047 | 21.327 | . 029 |  |
|  | 401/2 | $3^{\circ}-40^{\prime}$ | 3.567 | 23.336 | $22^{\circ}-00^{\prime}$ | 25.811 | 23.747 | . 035 |  |
| SWTTCH EASEMENT |  |  |  |  | 21/2-200. GAGE, |  |  | 5 FT | $41 / 2$ IN. |
| Point <br> No. | Cent. Rad. | Angle | Inner Rail |  | $\mathbf{S}^{\circ}$ | Length Outer | Length <br> Inner | Correction for T Rail | This Easement gives an $O$ G 0.250 greater and a G S 3.286 greater than Spiral No. $21 / 2$. |
|  |  |  | X | Y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.480 | 13.763 | $4^{\circ}-00^{\prime}$ | 14.151 | 13.775 | . 006 |  |
| 5 | 129 | $1^{\circ}-00^{\prime}$ | 0.654 | 15.962 | $5^{\circ}-00^{\prime}$ | 16.449 | 15.979 | . 008 |  |
| 6 | 74 | $2{ }^{\circ}-00^{\prime}$ | 0.914 | 18.436 | $7^{\circ}-00^{\prime}$ | 19.125 | 18.469 | . 011 |  |
| 7 | $631 / 2$ | $20^{\circ}-20^{\prime}$ | 1.265 | 20.888 | $9^{\circ}-20{ }^{\prime}$ | 21.821 | 20.945 | . 014 |  |
| 8 | $551 / 2$ | $2^{\circ}-40^{\prime}$ | 1.720 | 23.303 | $12^{\circ}-00^{\prime}$ | 24.529 | 23.403 | . 019 |  |
| 9 | 49 | $8{ }^{\circ}-00$ | 2.286 | 25.660 | $15^{\circ}-00^{\prime}$ | 27.236 | 25.828 | . 024 |  |
| 10 | 441/2 | $3{ }^{\circ}-20$ | 2.984 | 27.991 | $18^{\circ}-20^{\prime}$ | 28.981 | 28.261 | . 029 |  |
| 11 | 401/2 | $3^{\circ}-40^{\prime}$ | 3.817 | 30.262 | $23^{\circ}-00^{\prime}$ | 32.745 | 30.681 | . 035 |  |





| $\xrightarrow[\substack{\text { Point } \\ \text { No. }}]{\text { coser }}$ | $\underset{\substack{\text { Cent. } \\ \text { Rad. }}}{ }$ | Angle | Inner Rail |  | so | ${ }_{\substack{\text { Length } \\ \text { Outer }}}^{\text {col }}$ | ${ }_{\substack{\text { Length } \\ \text { Inner }}}^{\substack{\text { a }}}$ | $\begin{array}{\|l\|l\|} \substack{\text { toorrecer } \\ \text { toor } \\ \text { T Raii }} \end{array}$ | This Ease- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.480 | 13.763 | $4^{\circ}-00^{\prime}$ | 14.151 | 13.775 | . 006 | ment gives an $0 \quad \mathrm{G} 0.178$ |
| 4 | 1251/2 | $3^{\circ}-00^{\prime}$ | 1.097 | 20.162 | $7^{\circ}-00^{\prime}$ | 20.862 | 20.206 | . 011 | greater and |
| 5 | 84 | $3^{\circ}-30^{\prime}$ | 1.853 | 25.071 | $10^{\circ}-30^{\prime}$ | 26.158 | 25.172 | . 016 | G S equal to |
| 6 | 70 | $4^{\circ}-12^{\prime}$ | 2.929 | 29.885 | $14^{\circ}-42^{\prime}$ | 31.486 | 30.106 | . 023 | Spiral No. 4. |
| 7 | 60 | $4^{\circ}-54^{\prime}$ | 4.374 | 34.567 | $19^{\circ}-36$ | 36.847 | 35.009 | . 031 |  |



| Point | ${ }_{\text {cont }}^{\text {Cent. }}$ Rad. | Angle | Inner Rail |  | so | ${ }_{\substack{\text { Length } \\ \text { Outer }}}$ | $\underbrace{\substack{\text { a }}}_{\substack{\text { Length } \\ \text { Inner }}}$ |  | This Easement gives an |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | x | y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.480 | 13.763 | $4^{\circ}-00^{\prime}$ | 14.151 | 13.775 | . 006 | O G equal to |
| 4 | 144 | $1^{\circ}-00^{\prime}$ | 0.675 | 16.224 | $5{ }^{\circ}-00^{\prime}$ | 16.711 | 16.241 | . 008 |  |
| 5 | 120 | $2^{\circ}-30^{\prime}$ | 1.232 | 21.311 | $7^{\circ}-30^{\prime}$ | 22.064 | 21.360 | . 012 | than Spiral |
| 6 | 100 | $3^{\circ}-00^{\prime}$ | 2.028 | 26.344 | $10^{\circ}-30^{\prime}$ | 27.441 | 26.455 | . 016 | No. 5. |
| 7 | 85 - | $3^{\circ}-30^{\prime}$ | 3.095 | 31.256 | $14^{\circ}-00^{\prime}$ | 32.797 | 31.483 | . 022 |  |


| Point$\substack{\text { No. }}$Noser | Cent.Rad. | Angle | Inner Rail |  | So | Versine |  | Sine | $\underset{\substack{\text { Length } \\ \text { Outer }}}{ }$ |  | $\underset{\substack{\text { Length } \\ \text { Inner }}}{\text { cel }}$ | $\begin{aligned} & \text { Correc- } \\ & \text { tion for } \\ & \text { T Rail } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | X | Y |  |  |  |  |  |  |  |  |
| 1 <br> 2 <br> 3 <br> 4 <br> 4 <br> 5 <br> 8 <br> 7 | $\begin{aligned} & 900 \\ & 450 \\ & 300 \\ & 1850 \\ & 180 \\ & 150 \\ & 1128 \\ & 1121 / 2 \end{aligned}$ |  | 0.015 0.076 0.071 0.452 0.85 1.827 1.365 2.089 |  |  | .00002 .00015 .00011 .00391 .003745 .01324 |  | $\begin{aligned} & .00182 \\ & .0745 \\ & .03590 \\ & .0814 \\ & .108187 \\ & .162187 \end{aligned}$ |  |  |  | .001 .000 .003 .005 .000 .011 .015 |
| TIE ROD DISTANCES FROM P. S. |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & \text { Inner } \\ & \text { Rail } \end{aligned}$ | $\begin{aligned} & \text { Outer } \\ & \text { Raiil } \end{aligned}$ | $\begin{aligned} & \text { Inner } \\ & \text { Rail } \end{aligned}$ | $\begin{aligned} & \text { Outer } \\ & \text { Rai1 } \end{aligned}$ | $\begin{aligned} & \text { Inner } \\ & \text { Rail } \end{aligned}$ | $\begin{aligned} & \text { Outer } \\ & \text { Rail } \end{aligned}$ | $\begin{aligned} & \text { Inner } \\ & \text { Rai1 } \end{aligned}$ | $\begin{aligned} & \text { Outer } \\ & \text { Rail } \end{aligned}$ |  | $\begin{aligned} & \text { Inner } \\ & \hline \text { Rail } \end{aligned}$ | $\begin{aligned} & \text { Outer } \\ & \text { Rail } \end{aligned}$ | Inner | Outer Rail |
| $\begin{aligned} & 1.00 \\ & \hline 1.99 \\ & \hline .99 \\ & \hline .99 \\ & \hline 5.99 \\ & 5.98 \end{aligned}$ | 1.00 1.00 2.01 3.01 4.01 5.01 6.01 602 | ( 6.97 | ( ${ }^{\text {7.03 }}$ | (12.93 | 13.07 14.08 15.08 15.09 16.10 17.11 18.12 | $\begin{aligned} & 18.87 \\ & 19.86 \\ & 20.84 \\ & 21.83 \\ & 22.81 \\ & 23.81 \\ & 23.80 \end{aligned}$ | 19.13 20.14 20.14 21.16 22.17 23.19 24.20 |  | $\begin{aligned} & 24.78 \\ & 2.78 \\ & 26.72 \\ & 20.78 \\ & 28.71 \\ & 2.71 \end{aligned}$ |  |  |  |


|  | WI | H | SEM | NT | 6-200 | GA | E, 5 | FT. 4 | IN. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Point No. | Cent. Rad. | Angle | Inner Rail |  | $S^{\circ}$ | Length Outer | Length Inner | Correction for T Rail | This Ease- |
|  |  |  | X | Y |  |  |  |  |  |
|  | 200 | $4^{\circ}-00^{\prime}$ | 0.480 | 13.763 | $4^{\circ}-00^{\prime}$ | 14.151 | 13.775 | . 006 | O G equal to |
| 5 | 255 | $1^{\circ}-00^{\prime}$ | 0.827 | 18.154 | $5^{\circ}-00^{\prime}$ | 18.648 | 18.178 | . 008 |  |
| 6 | 150 | $2{ }^{\circ}-00^{\prime}$ | 1.365 | 23.267 | $7{ }^{\circ}-00^{\prime}$ | 23.977 | 23.321 | . 011 | Spiral No. 6. |
| 7 | 128 | $2^{\circ}-20^{\prime}$ | 2.089 | 28.319 | $9^{\circ}-20^{\prime}$ | 29.300 | 28.424 | . 015 |  |

## Middle Ordinates

for
10-Foot Chords.

## Middle Ordinates， 10 Ft．Chords

| м． 0. | dius | м．o． | adius | м．о． | Radius |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | infinity |  | 150＇－ |  |  |
|  | ${ }^{4807^{\prime}-8{ }^{\prime \prime}}$ | ${ }^{11_{18}{ }^{18}}$ | ${ }^{1455^{\prime}} 14{ }^{6}$ | $2{ }^{16}$ |  |
| ${ }^{18}$ | 1600＇${ }^{10 \prime \prime}$ |  | $133^{\prime \prime}-233^{\prime \prime}$ $133^{\prime \prime}-43^{\prime \prime}$ | 2 ${ }^{\frac{1}{4} 8^{\prime \prime}}$ |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  | ${ }_{120}^{123}$ |  |  |
| 尔＂ | 533＇－41／8＂ | ${ }_{\text {1 }}^{\text {告＂}}$ | 117＇－1／8＇${ }^{\prime \prime}$ | $2_{\text {2a }}^{\text {a }}$ | $65^{\prime}$ |
|  | $480{ }^{\circ}-$ | $1{ }^{\text {5 }}$ | 114＇－ | $2{ }^{\frac{5}{4} 0^{\prime \prime}}$ |  |
| 彦＂ |  | 11新＂ | ${ }^{1111^{\prime}-}$ |  |  |
|  | ${ }^{369}{ }^{\prime}$ | ${ }^{13_{3} 8^{2}}$ |  | 2 |  |
| $\stackrel{\text { \％}}{18}$ | 342＇－10 ${ }^{\text {5 }}{ }^{\text {² }}$ | ${ }^{1+\frac{7}{18}}$ | 104＇－ 4 48＂ | 2 2\％＂ | 61＇ |
|  | $320^{\prime}-0$ | $1{ }^{155^{\prime \prime}}$ | 102＇－2 | ${ }^{215^{2} \underline{5}^{\prime}}$ |  |
|  | ${ }^{300}{ }^{\prime}$ |  | 100＇－0 |  |  |
|  |  |  | ${ }_{96}{ }^{9}$－ |  |  |
|  |  |  | 94＇－ 2 $_{\text {樹＂}}{ }^{\prime \prime}$ |  | 57＇－11／4 |
|  | 240 |  | $92^{\prime}$－ | 258＂ | 57＇－3＂ |
|  | ${ }^{228} 8^{\prime \prime}$ | 121 | 90＇－7 | ${ }^{2}$ |  |
|  | 209＇－ |  | $8{ }^{1}$ | 2 |  |
|  |  |  |  |  |  |
| 8 | 192 |  | 84－${ }^{\text {1／}}$ | ${ }^{2 \frac{3}{3} \frac{3}{2}^{\prime \prime}}$ |  |
|  | 184 |  | 82 |  |  |
|  | 171＇－51\％${ }^{1 / 2}$ |  | 80＇，01 | 2\％ |  |
|  | 165＇－635＂ |  | 788，93， | ${ }_{2}^{2}$ |  |
| \％ |  |  | 76－314＂ | 2igi＂ | 1 |

## Middle Ordinates， 10 Ft．Chords

| м．о． | Radius | M．o． | Radius | м．о． | Radius |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $3^{\prime \prime}$ |  |  |  |  |  |
|  |  | ${ }_{\text {4，}}^{4 \times 10}$ |  |  |  |
| 31／4＂ |  |  |  |  |  |
|  | 47＇－77／${ }^{\prime \prime}$ |  | 36＇－ |  |  |
|  | 47＇－${ }^{\text {cin }}$ |  | $35^{\circ}-11{ }^{\text {a }}$ | －${ }_{\text {ckig }}$ |  |
|  |  | ${ }^{4} 4$ | $\xrightarrow{35-8,}{ }^{3514}$ |  |  |
| $3^{\frac{3}{88}}$ |  | $4{ }_{38}{ }^{\text {² }}$ |  | $5{ }^{\text {ctig }}$ |  |
|  | $45^{\prime}$ | $4{ }^{5}$ | $34^{4}$－ | $5_{5}^{5}$ | 28 |
|  | 44 | ${ }_{4}^{43}$ |  | 年产＂ |  |
|  | 44 | ${ }^{418}$ |  |  |  |
| ${ }^{3}{ }^{\frac{1}{18}}$ | 43＇－ $9388^{\prime \prime}$ | $4^{13^{\prime \prime}}$ | 33 | $5_{18}{ }^{\frac{7}{4 \prime \prime}}$ |  |
| $3{ }^{35^{\text {ax }}}$ | 43＇－ | 4185＂ | 33＇ | 515\％ |  |
|  | ${ }_{42-1}^{43-0}$ | ${ }^{4}$ | －$33-6$ <br> $33-1$ | 512＂ |  |
|  | 42＇ |  | 33＇－ 0 | \％．9\％ |  |
| ${ }_{317}{ }^{1 / 4}$ | 41＇－101018 |  | 32 |  |  |
|  | ${ }^{411^{\prime}-63}$ | 458＂ | 33＇－ | 558＂ |  |
|  | ${ }^{41-10^{2} 8^{8}}$ |  | － | ¢ |  |
|  | 40＇－ $57 /{ }^{\prime \prime}$ |  | 31＇－11＋${ }^{\text {d }}$ | 5竦 |  |
|  |  | ${ }_{4}^{434^{2}}{ }^{\text {a }}$ |  | ${ }^{534^{\text {a }} \text {＂}}$ |  |
|  |  |  |  |  |  |
|  |  | 4iziv |  |  |  |
| 边 | －${ }_{38}^{38-10}$ | ${ }^{475^{\prime \prime}}$ | $\xrightarrow{30}{ }^{\circ}{ }^{\circ}-1$ |  |  |
| ${ }^{3}$ |  |  |  | 5 |  |
| $3_{3}^{\text {a }}$ | 37＇－11／2＂ | $4{ }^{\frac{1}{3} \bar{y}^{\prime \prime}}$ | 30＇－43＂ |  | 4 |

## Wheel Contours



GREAT variety of wheel contours are used on street railways, and often the extremes are used on the same track system to the great detriment of both special work and wheels.

Since there are now no standard wheel contours except the M. C. B. (steam rai1road), it seems proper to offer some designs which will meet most of the difficulties found in our practice.

The contour of wheel fixes the character of the special work as to whether the frog work is to be "flange bearing." This term means that at the "waist of frog," i. e., just in advance of the point of frog, the floor of the throat is raised to carry the wheel through the waist and past the point upon its flange. The latter cannot be of a shape or character of metal well adapted to this service, and more or less chipped flanges are thereby caused. It is, however, inevitable that this support be provided,
unless the tread is wide enough to carry the wheel past this critical point.

Contour " $A$ " is the M. C. B. standard wheel, and is adapted to open track and streets where rails with deep and wide flangeways are provided, and the paving is such that the tread will not be seriously chipped by contact with the same.

Contour " B " is a compromise wheel, for use where a portion of the track system is used by wheels having Contour " A " and the remainder has not the deep flangeway, but the width of flangeway is provided. If the paving conditions of this .portion are such that the width of tread must be reduced from that shown, all frog work on the entire portion of system used by Contour "B" must be made "flange bearing."

Contour " C " is adapted to track systems where wide and deep flangeways cannot be provided but the paving conditions are such that the width of the tread shown can be used.

Contour " D " is adapted to track systems where a narrower tread is required by
the paving conditions, the shape and size of flange being the same as "C." As wide a tread as possible should be used, as the life of special work will thereby be materially prolonged besides increasing the factor of safety on any open track in the system. "Flange-bearing" frogs will be required for this contour.

Contours "A" and, "C" will give the best results where conditions permit their use and do not require "flange-bearing" frogs.

Contour "B" will not give entire satisfaction, since the flange is not of the best shape, and should only be used when compelled by the conditions stated.

Contours "C" and "D" can be used on the same track system if "flange-bearing" frogs are provided for that portion on which Contour " D " is used.

Contours " $C$ " and " $D$ " cannot" be satisfactorily used on track systems designed for Contours "A" or "B," or vice versa.



Frog and Switch Department of The Pennsylvania Steel Company, Steelton, Pa.

## Angles

Bulb

> Reinforcing
> Switch
Equal Legs
Unequal Legs

Braces
Acme
Switch
Guard
Interlocking
Tie Plate
Bridges
Buildings
Chairs
Rail chairs for steam railroads in paved streets

## Channels

## Circles

Turntables
Coal storage tracks

## Clamps

Guard rail

## Crossings

Bolted
Bolted Plate
Keyed
"Manard" Steel
Movable Point
Riveted
Street Railway
"Manard" Renewable Centre
Double Slip
Single Slip
Three Rail


Drop Forged Socket


Acme Brace


Manard Anvil Face Frog, Design 153


Manard Anvil Face Spring Rail Frog

## Crossovers

Single Crossovers<br>Double Crossovers<br>Portable Crossovers

## Forgings

Frogs, Rigid

Bolted
Bolted Plate
Keyed
"Manard" Steel
"Manard" Renewable Centre Riveted
Frogs, Spring
Bolted
Bolted Plate
Double
Hinged
Keyed
"Manard" Steel
Riveted Plate
Twin
Vaughan Hinged
Vaughan Sliding
Joints
Angle
Channel
Compromise
Deep Girder Rail
Plain
Knees
Mates.
Built
" Manard" Bolted
"Manard " Key Fast

## Plates

. Frog
Slide
Switch

Tie
Rails, Guard


Manard Grooved Tongue Switch for Steam Railloads in Paved Streets



Rapid Renewable Manard Centre Frog

## Rails

A. S. C. E. Sections

Cast Weld Compromise
Check
Flat
Girder
Girder Guard
Slot Rails and Conductor Bars
Tee
High Tee
Tram
Rails, Renewable Guard
Rods, Switch Connecting
Splice Bars
Spikes
Spiral Curves
Steam Railroad Track Equipment
Street Railway Special Work
Street Railway Track Fastenings
Steel
Bessemer
Billets
Blooms
Castings
Forgings
Flats
Basic Open Hearth Acid Open Hearth
"Manard "
Merchant
Round
Shapes
Slabs
Special
Square
Tool
Structural Steel

Standard Manard Big Pin Switch

92 THE PENNSYLVANIA STEEL COMPANY


Ground Lever, Model 16


Low New Century Adjustable Switch Stand Model 51 A


Intermediate Main Line Switch Stand Model 4; B

## Switches

Adjustable
Angle
Challenge
Lorenz
"Manard" Big Pin Grooved Tongue
"Manard" Big Pin Tongue
"Manard" Steel Plain

Reinforced
Socket
Stub
Three Way

## Switch Stands

Automatic
Banner
Steelton Detective
Ground Levers
Upright Levers
Long Safety
Main Line Adjustable
Positive
Automatic
Mine
Mine Kickover
New Century
New Century Adjustable
New Era
Pet
Semaphore with disappearing blade
Spring Ground Throw
Yard Stands
Tie Plates
Tie Rods
Track Bolts
Track Fastenings
Track Girders
Track Material of All Kinds
Trough Floors
Trough Sections
Viaducts
" Z" Bars



Chasmar-Winchell Press New York and Pittsburgh

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